

Date _____ Calc. _____ Chkd. _____ Appr. _____

Software by SANT'AMBROGIO S.I. srl - Milano, Italy - EN Rev. 1.24-Jgv/aUs

CYLINDRICAL SHELL POS.: 1

According to EN 13445-3 Ed. 2002 up to issue 21 (Clause 7 - 8)

* Design temperature $T = 150.0 \text{ }^{\circ}\text{C}$
 * MATERIAL : (Rec.Nr 119) SA 516 Gr. 60 PMA REQUIRED
 * NOMINAL DESIGN STRESS-DESIGN $f = 129.91 \text{ MPa}$
 * NOMINAL DESIGN STRESS-AT ROOM TEMPERATURE $f_A = 147.33 \text{ MPa}$
 * NOMINAL DESIGN STRESS-HYDRAULIC TEST $f_{test} = 210.48 \text{ MPa}$

----- CHECK UNDER INTERNAL PRESSURE (EN 13445-3 Clause 7.4.2) -----
 Design pressure $P' = 1.400 \text{ MPa}$
 Test pressure $p_t' = 2.350 \text{ MPa}$
 Overpressure due to static head - Design $p_h' = 0.000 \text{ MPa}$
 Overpressure due to static head - test $p_{ht}' = 0.000 \text{ MPa}$
 Calculation pressure - Design $p = p_h' + p' = 1.400 \text{ MPa}$
 calculation pressure - Test $p_t = p_{ht}' + p_t' = 2.350 \text{ MPa}$
 Shell internal diameter $D_i = 610.00 \text{ mm}$
 Joint efficiency $z = 1.00$
 Corrosion allowance $c = 3.00 \text{ mm}$
 Wall undertolerance ($\delta_M + \delta_E$) $\delta = 0.00 \text{ mm}$
 Adopted thickness $e_n = 10.00 \text{ mm}$
 * DESIGN : $e = p \cdot (D_i + 2c + 2\delta) / (2 \cdot f \cdot z - P) + c + \delta = 6.337 \text{ mm}$
 * TEST : $e = p_t \cdot (D_i + 2\delta) / (2 \cdot f_{test} - P_t) + \delta = 3.424 \text{ mm}$

----- PRESSURES -----
 MAX. DESIGN PRESSURE - INTERNAL $= 2.919 \text{ MPa}$
 MAX. TEST PRESSURE - INTERNAL $= 6.790 \text{ MPa}$
 - INTERNAL: $1.43 \cdot P'$ $= 2.002 \text{ MPa}$
 SHELL - INTERNAL: $1.25 \cdot P' \cdot f_A / f = 1.985 \text{ MPa}$

Date _____ Calc. _____ Chkd. _____ Appr. _____

Software by SANT'AMBROGIO S.I. srl - Milano, Italy - EN -Rev. 1.24-QGbB/aUs
OPENING REINFORCEMENT POS.: 12
According to EN 13445-3 Ed. 2002 up to issue 21 (Clause 9)

* Design temperature T = 150.0 °C

* NOZZLE

* MATERIAL :(Rec.Nr 168) SA 333 Gr. 6 PMA REQUIRED

* NOMINAL DESIGN STRESS-DESIGN fb= 142.57 MPa

* NOMINAL DESIGN STRESS-AT ROOM TEMPERATURE fbA= 160.67 MPa

* NOMINAL DESIGN STRESS-HYDRAULIC TEST fbTest= 229.52 MPa

* PAD

* MATERIAL :(Rec.Nr 168) SA 333 Gr. 6 PMA REQUIRED

* NOMINAL DESIGN STRESS-DESIGN fp= 142.57 MPa

* NOMINAL DESIGN STRESS-HYDRAULIC TEST fpTest= 229.52 MPa

* SHELL DATA

| | |
|---------------------|---------------|
| Internal diameter | D = 610.00 mm |
| Thickness | en = 10.00 mm |
| Joint efficiency | z = 1.00 |
| Corrosion allowance | c = 3.00 mm |
| wall undertolerance | δ = 0.00 mm |

* NOZZLE DATA

| | |
|---|---------------------------|
| Type of connection : | Protruding |
| Outside diameter | deb= 168.30 mm |
| Thickness | eb= 14.27 mm |
| Joint efficiency | zb= 1.00 |
| Corrosion allowance | cb= 3.00 mm |
| Wall undertolerance | δb= 0.00 mm |
| Internal protruding | lbi= 0.00 mm |
| Pad thickness | ep= 10.00 mm |
| Pad width | lp= 75.85 mm |
| Useful length (Horizontal limit to nozzle OD) | ls= 300.00 mm |
| Useful length (Vertical limit to shell OD) | lb= 108.40 mm |
| Nozzle position: | Normal to the wall |
| Angular coordinate of nozzle | γ = 0.00 ° |
| Distance from line | Z = 300.00 mm |
| Weld areas | Afw = 237 mm ² |
| Value from fig. EN 13445-3 9.4-14 (design) | Maxeb/en = 2.000 |
| Nozzle calculat.thk. $eb^* = \min(eb - cb - \delta b, \max eb / en(en - c - \delta))$ | = 11.27 mm |
| Value from fig. EN 13445-3 9.4-14 (test) | Maxeb/en = 2.000 |
| Nozzle calculat.thk. $eb^* = \min(eb - \delta b, \max eb / en(en - \delta))$ | = 14.27 mm |

Opening is a critical area as defined in clause 17

----- PRESSURES -----

| | |
|---|-------------|
| MAX. DESIGN PRESSURE - INTERNAL | = 4.892 MPa |
| MAX. TEST PRESSURE - INTERNAL | = 9.937 MPa |
| - INTERNAL: $1.43 \cdot P'$ | = 2.002 MPa |
| NOZZLE - INTERNAL: $1.25 \cdot P' \cdot fbA / fb$ | = 1.972 MPa |

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OPENING REINFORCEMENT POS.: 12
According to EN 13445-3 Ed. 2002 up to issue 21 (Clause 9)

----- CHECK UNDER INTERNAL PRESSURE: DESIGN -----

| | | | |
|---------------------------------|------------------|-------|-----|
| Pressure | $p' =$ | 1.400 | MPa |
| Overpressure due to static head | $p'' =$ | 0.000 | MPa |
| Calculation pressure | $p = p' + p'' =$ | 1.400 | MPa |

| | | | |
|---|---|---------|-----------------|
| Shell internal diameter | $Di = D + 2 \cdot c + 2 \cdot \delta =$ | 616.00 | mm |
| $ea, s = en - c - \delta$ | $=$ | 7.00 | mm |
| $lso = \text{SQR}((Di + ea, s)(ea, s))$ | $=$ | 66.04 | mm |
| $ls' = \text{MIN}(lso, ls)$ | $=$ | 66.04 | mm |
| $Lp' = \text{MIN}(lso, lp)$ | $=$ | 66.04 | mm |
| $lbo = \text{sqr}((deb - eb*)(eb*))$ | $=$ | 42.07 | mm |
| $lb' = \text{MIN}(lbo, lb)$ | $=$ | 42.07 | mm |
| $lbi' = \text{MIN}(0.5 \cdot lbo, lbi)$ | $=$ | 0.00 | mm |
| $Aps = (Di/2)(ls' + deb/2)$ | $=$ | 46257.9 | mm ² |
| $Afs = ls'(ea, s)$ | $=$ | 462.3 | mm ² |
| $Afp = ep \cdot Lp'$ | $=$ | 660.4 | mm ² |
| $Apb = .5 \cdot (deb - 2eb + 2cb + 2\delta b) \cdot (lb' + ea, s)$ | $=$ | 3576.1 | mm ² |
| $Afb = (lb' + en - cb)(eb*)$ | $=$ | 553.0 | mm ² |
| $(Afs + Afb)(f - .5 \cdot p) + (Afp)(f - .5 \cdot p) + Afb(f - .5 \cdot p)$ | $=$ | 247130 | N |
| $(Aps + Apb) \cdot p$ | $=$ | 69768 | N |

----- CHECK UNDER INTERNAL PRESSURE: TEST -----

| | | | |
|---------------------------------|------------------|-------|-----|
| Pressure | $p' =$ | 2.350 | MPa |
| Overpressure due to static head | $p'' =$ | 0.000 | MPa |
| Calculation pressure | $p = p' + p'' =$ | 2.350 | MPa |

| | | | |
|--|-----------------------------|---------|-----------------|
| Shell internal diameter | $Di = D + 2 \cdot \delta =$ | 610.00 | mm |
| $ea, s = en - \delta$ | $=$ | 10.00 | mm |
| $lso = \text{SQR}((Di + ea, s)(ea, s))$ | $=$ | 78.74 | mm |
| $ls' = \text{MIN}(lso, ls)$ | $=$ | 78.74 | mm |
| $lbo = \text{sqr}((deb - eb*)(eb*))$ | $=$ | 46.88 | mm |
| $lb' = \text{MIN}(lbo, lb)$ | $=$ | 46.88 | mm |
| $lbi' = \text{MIN}(0.5 \cdot lbo, lbi)$ | $=$ | 0.00 | mm |
| $Aps = (Di/2)(ls' + deb/2)$ | $=$ | 49681.5 | mm ² |
| $Afs = ls'(ea, s)$ | $=$ | 787.4 | mm ² |
| $Afp = ep \cdot Lp'$ | $=$ | 758.5 | mm ² |
| $Apb = .5 \cdot (deb - 2eb + 2\delta b) \cdot (lb' + ea, s)$ | $=$ | 3975.0 | mm ² |
| $Afb = (lb' + en)(eb*)$ | $=$ | 811.7 | mm ² |
| $(Afs + Afb)(f_{test} - .5 \cdot p) + (Afp)(f_{test} - .5 \cdot p) + Afb(f_{test} - .5 \cdot p)$ | $=$ | 543038 | N |
| $(Aps + Apb) \cdot p$ | $=$ | 126093 | N |